F_y = 36 ksi
F_u = 58 ksi

Table 5-2 (continued)
Available Strength in Axial Tension
Angles

L7–L5

Shape	Gross Area, A_g	A_e = 0.75A_g	Yielding kips		Rupture kips	
			P_n/Ω_t	$\phi_t P_n$	P_n/Ω_t	$\phi_t P_n$
	in.²	in.²	ASD	LRFD	ASD	LRFD
L7×4×3/4	7.74	5.81	167	251	168	253
×5/8	6.50	4.88	140	211	142	212
×1/2	5.26	3.95	113	170	115	172
×7/16	4.63	3.47	99.8	150	101	151
×3/8	4.00	3.00	86.2	130	87.0	131
L6×6×1	11.0	8.25	237	356	239	359
×7/8	9.75	7.31	210	316	212	318
×3/4	8.46	6.35	182	274	184	276
×5/8	7.13	5.35	154	231	155	233
×9/16	6.45	4.84	139	209	140	211
×1/2	5.77	4.33	124	187	126	188
×7/16	5.08	3.81	110	165	110	166
×3/8	4.38	3.29	94.4	142	95.4	143
×5/16	3.67	2.75	79.1	119	79.8	120
L6×4×7/8	8.00	6.00	172	259	174	261
×3/4	6.94	5.21	150	225	151	227
×5/8	5.86	4.40	126	190	128	191
×9/16	5.31	3.98	114	172	115	173
×1/2	4.75	3.56	102	154	103	155
×7/16	4.18	3.14	90.1	135	91.1	137
×3/8	3.61	2.71	77.8	117	78.6	118
×5/16	3.03	2.27	65.3	98.2	65.8	98.7
L6×3 1/2×1/2	4.50	3.38	97.0	146	98.0	147
×3/8	3.44	2.58	74.2	111	74.8	112
×5/16	2.89	2.17	62.3	93.6	62.9	94.4
L5×5×7/8	8.00	6.00	172	259	174	261
×3/4	6.98	5.24	150	226	152	228
×5/8	5.90	4.43	127	191	128	193
×1/2	4.79	3.59	103	155	104	156
×7/16	4.22	3.17	91.0	137	91.9	138
×3/8	3.65	2.74	78.7	118	79.5	119
×5/16	3.07	2.30	66.2	99.5	66.7	100

Limit State	ASD	LRFD
Yielding	$\Omega_t = 1.67$	$\phi_t = 0.90$
Rupture	$\Omega_t = 2.00$	$\phi_t = 0.75$

Note: Tensile rupture on the effective net area will control over tensile yielding on the gross area unless the tension member is selected so that an end connection can be configured with $A_e \geq 0.745A_g$.

L5–L3 1/2

Table 5-2 (continued)
Available Strength in Axial Tension
Angles

F_y = 36 ksi
F_u = 58 ksi

Shape	Gross Area, A_g	A_e = 0.75A_g	Yielding kips P_n/Ω_t	Yielding kips $\phi_t P_n$	Rupture kips P_n/Ω_t	Rupture kips $\phi_t P_n$
	in.²	in.²	ASD	LRFD	ASD	LRFD
L5×3 1/2×3/4	5.85	4.39	126	190	127	191
×5/8	4.93	3.70	106	160	107	161
×1/2	4.00	3.00	86.2	130	87.0	131
×3/8	3.05	2.29	65.7	98.8	66.4	99.6
×5/16	2.56	1.92	55.2	82.9	55.7	83.5
×1/4	2.07	1.55	44.6	67.1	45.0	67.4
L5×3×1/2	3.75	2.81	80.8	122	81.5	122
×7/16	3.31	2.48	71.4	107	71.9	108
×3/8	2.86	2.15	61.7	92.7	62.4	93.5
×5/16	2.41	1.81	52.0	78.1	52.5	78.7
×1/4	1.94	1.46	41.8	62.9	42.3	63.5
L4×4×3/4	5.44	4.08	117	176	118	177
×5/8	4.61	3.46	99.4	149	100	151
×1/2	3.75	2.81	80.8	122	81.5	122
×7/16	3.30	2.48	71.1	107	71.9	108
×3/8	2.86	2.15	61.7	92.7	62.4	93.5
×5/16	2.40	1.80	51.7	77.8	52.2	78.3
×1/4	1.93	1.45	41.6	62.5	42.1	63.1
L4×3 1/2×1/2	3.50	2.63	75.4	113	76.3	114
×3/8	2.68	2.01	57.8	86.8	58.3	87.4
×5/16	2.25	1.69	48.5	72.9	49.0	73.5
×1/4	1.82	1.37	39.2	59.0	39.7	59.6
L4×3×5/8	3.99	2.99	86.0	129	86.7	130
×1/2	3.25	2.44	70.1	105	70.8	106
×3/8	2.49	1.87	53.7	80.7	54.2	81.3
×5/16	2.09	1.57	45.1	67.7	45.5	68.3
×1/4	1.69	1.27	36.4	54.8	36.8	55.2
L3 1/2×3 1/2×1/2	3.25	2.44	70.1	105	70.8	106
×7/16	2.89	2.17	62.3	93.6	62.9	94.4
×3/8	2.50	1.88	53.9	81.0	54.5	81.8
×5/16	2.10	1.58	45.3	68.0	45.8	68.7
×1/4	1.70	1.28	36.6	55.1	37.1	55.7

Limit State	ASD	LRFD
Yielding	$\Omega_t = 1.67$	$\phi_t = 0.90$
Rupture	$\Omega_t = 2.00$	$\phi_t = 0.75$

Note: Tensile rupture on the effective net area will control over tensile yielding on the gross area unless the tension member is selected so that an end connection can be configured with $A_e \geq 0.745A_g$.